

This appendix was initially prepared to document supported details for the Delta Conveyance Project (Project) Engineering Project Reports, (DCA 2022). At that time of submittal in 2022, the Delta Conveyance Authority (DCA) prepared two Engineering Project Reports, one report with the Central Corridor and Eastern Corridor and one report with the Bethany Reservoir Alternative. In December 2023, the Environmental Impact Statement (EIR) (DWR, 2023) was released and stated that the Bethany Reservoir Alternative would be the selected Project and renamed the Bethany Reservoir Alignment.

In September 2024, this appendix was updated to describe the Project selected by DWR, the Bethany Reservoir Alignment. No technical changes are presented since Final Draft Submittal in 2023 (DCA, 2023). This appendix presents the results of facilities siting studies based upon locations for tunnel shafts for the Central Corridor, Eastern Corridor (or East Corridor), and Bethany Reservoir Alignment. Although the Central Corridor is no longer part of the Delta Conveyance Project, the conditions considered for the Central Corridor influenced the locations of tunnel shafts evaluated for the Eastern Corridor and Bethany Reservoir Alignment. With respect to the Eastern Corridor, the siting evaluations for the tunnel shafts from Twin Cities Complex to Lower Roberts Island were used specifically for the Bethany Reservoir Alignment. Therefore, information for the siting studies for the Central and Eastern corridors were included in this appendix.

h .

The Bethany Reservoir Alignment of the Delta Conveyance Project (Project) would include intakes along the Sacramento River between the confluences with American River and Sutter Slough. It would also include a tunnel between the intakes and the Bethany Reservoir Pumping Plant (BRPP), which would pump the water directly into the existing Bethany Reservoir. A Surge Basin would be constructed immediately upstream of the pumping plant to contain flow from a hydraulic surge event during operations. The pumping plant would discharge flow through the Bethany Reservoir Aqueduct (Aqueduct), comprised of four large-diameter pipelines connecting to the Bethany Reservoir.

The purpose of this technical memorandum (TM) is to document methods used to identify and evaluate potential sites for intakes, shafts, BRPP, Surge Basin, and Aqueduct, the criteria used for the evaluations, and recommendations for the preferred location of each facility.

The details regarding the selection of intake and launch shaft locations for the Bethany Reservoir Alignment are identical to those described for the Central and Eastern corridors in the Delta Conveyance Project Concept Engineering Report (CER) B6 Intake Site Identification and Evaluation and CER Appendix C5 Shaft Siting Study, respectively. The logic behind the selection of the maintenance and reception shaft locations is also identical to the Central and Eastern corridors, as described in CER Appendix C5 Shaft Siting Study; however, some additional locations were considered, as discussed in more detail here. Where appropriate, descriptions of features and processes that are unchanged from the CER Appendix B6 Intake Site Identification and Evaluation will be provided by reference only.

The Bethany Reservoir Alignment was determined to be most compatible with the Eastern corridor, since the tunnel launch from Lower Roberts Island can excavate a tunnel directly to the BRPP Surge Basin reception shaft within the 15-mile-maximum threshold established for the Project, whereas the

| Facilities Siting Study (Final Draft) |) | ·# |) | · ·# | • • | |
|--|---------------|--------------|---------------|------------|-------------------|--------|
| , | , | | , | | #-k ° |) . |
| tunnel drive length from Bouldin Island o | on the Cent | ral corrido | or would exc | eed 15 mi | iles. As such, t | he |
| Bethany Reservoir Alignment following t | he Central | corridor w | ould have r | equired ar | n additional tu | ınnel |
| drive in the South Delta which was consi | dered too i | mpactful f | for further e | valuation | due to the inc | reased |
| impacts to traffic, natural resources, hab | itat, air qua | ality, and t | he nearby c | ommuniti | es. | |

This TM is organized as follows:

- Introduction and Purpose
- Organization
- Intake Location Siting Study
- Launch Shaft Siting Study
- Maintenance and Reception Shaft Siting Study
- Bethany Reservoir Pumping Plant and Surge Basin Siting Study
- Selection of Bethany Reservoir Aqueduct Alignment (Route Study)
- Selection of Road Traffic Modification Locations
- Selection of Rail-Served Material Depot Locations
- References
- Attachment 1: Maintenance/Reception Shaft Siting Study
- Attachment 2: Bethany Reservoir Pumping Plant and Surge Basin Siting Study
- Attachment 3: Bethany Reservoir Aqueduct Alignment Siting Study
- Attachment 4: Bethany Reservoir Haul Route Alignment Study

| @ | .O | Ö | Ö | • |
|---|----|---|---|---|
| | | | | |

Recommended intake locations for the Project are identical to those discussed in the CER Appendix B6 *Intake Site Identification and Evaluation*.

0 0 0 0

Recommended launch shaft locations for the Bethany Reservoir Alignment are discussed in CER Appendix C5 Shaft Siting Study.

 $\mathsf{U} \qquad \mathsf{k} \qquad \mathsf{o} \quad \mathsf{o} \quad \mathsf{o}$

Recommended reception and maintenance shaft locations for the Bethany Reservoir Alignment are discussed in CER Appendix C5 Shaft Siting Study.

" k h h o " o

The Bethany Complex refers to the combined elements at the southern end of the Project, including the BRPP, Surge Basin, Bethany Reservoir Aqueduct (Aqueduct), and discharge and control structures at Bethany Reservoir. One of the primary portions of Bethany Complex would include the BRPP to convey water to the Bethany Reservoir, a Surge Basin to contain flow from a hydraulic surge event during operations, and surge tanks to manage hydraulic surge within the Aqueduct pipelines. The Bethany Complex would also include the Aqueduct connecting the BRPP to Bethany Reservoir and the discharge structure at the reservoir. This section focuses on siting the BRPP and Surge Basin since they would influence the location of the other features in the Bethany Complex.

The purpose of the BRPP would be to lift flows to a hydraulic gradeline sufficient for delivery into Bethany Reservoir, which operates at approximately elevation 245 feet above sea level. Accordingly, the BRPP would connect to the Aqueduct, consisting of four pressurized pipelines to the Bethany Reservoir. The purpose of the Surge Basin is to provide an overflow catchment basin at the end in the tunnel between the intakes and the BRPP to mitigate transient surge pressures.

8 o " k h h o " '

The BRPP and Surge Basin would generally need to be located between the southern edge of the Clifton Court Forebay (CCF) and the northern or eastern edge of Bethany Reservoir. The Surge Basin would need to be located where the topography would support a catchment with a bottom elevation near 0 to 10 feet to be compatible with the hydraulic gradeline within the tunnel. The Surge Basin and BRPP would not have to share a common location, but if separated, the pumping plant could require additional surge control features in the wet well.

The area for siting is occupied by multiple canals, high-voltage overhead transmission lines, high-pressure gas and petroleum lines, a major energy facility, the existing Jones (CVP) and Harvey O. Banks (State Water Project [SWP]) pumping plants, a highway, school, and multiple conservation easements. The terrain is relatively flat and close to sea level near the CCF but rises steadily and becomes more rolling terrain to the south and reaches elevations over 300 feet in some areas near Bethany Reservoir. Other than the facilities listed, most of the land is open space or used for agricultural production. Attachment 2.1 depicts the overall area considered for siting the BRPP and Surge Basin.

Establishing potential sites for the BRPP and Surge Basin focused on five primary goals:

- The BRPP and Surge Basin would need to be located on a relatively large site (75 acres or more) to allow adequate space for construction equipment and material storage and staging areas. The site would need to be located on relatively flat terrain and would need to be compatible with adjacent topography for conveyance routes to the reservoir.
- 2) # For conventional surface configurations, the BRPP would need to be located on relatively lower elevation sites because of limitations in the length of pump shafts to reach the water in the tunnel deep underground (operating water surfaces as low as elevation -50 to -60 feet). Additionally, the site elevation would ideally be compatible with a conventionally excavated Surge Basin. If the Surge Basin catchment area was below the existing grade, that would eliminate the need for construction of above grade embankments and not require the surge basin to fall under the Division of Safety of Dams jurisdiction.
- 3) 7 # k Approximately one-third of the northern and eastern sides of Bethany Reservoir are formed by dams or embankments. It is not desirable to connect to the reservoir through these structures. Therefore, the BRPP would need to be located so there is a reasonable conveyance route to the reservoir where outlet construction can avoid existing dams or embankments.
- 4) u The BRPP and Surge Basin location would need to be compatible with the Lower Roberts Island launch site and the upstream tunnel and shaft locations. This would include limiting the length to 15 miles as well as the need for an acceptable reception shaft location

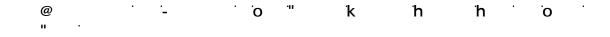
at the BRPP and Surge Basin site as part of the surge overflow scheme. The rationale for associating the Bethany Reservoir Alignment to the Eastern Corridor is discussed in further detail in Section 7.3.

" k " - "u " o "# "

Initial consideration of the Bethany Reservoir Alignment included both the Central and Eastern Corridors. Material presented in Section 5 covers this topic in part, but additional context is provided below.

The choice between the Central and Eastern Corridors for the Bethany Reservoir Alignment is primarily a function of tunnel length and whether shafts would need to be added in either scenario. The more favorable geotechnical conditions, cost, and complexity of constructing shafts (particularly tunnel launch shafts) and access to the launch shaft sites creates a clear advantage for the Eastern Corridor. In order to associate the Bethany Reservoir Alignment to the Central Corridor without adding a launch shaft, it would be necessary to tunnel from the planned launch shaft at Bouldin Island. This, however, is about 20 miles from the Surge Basin, which is too far for a single bore. Alternatively, the bore could be between Bacon Island and the Surge Basin, but Bacon Island is planned for a reception shaft because it is too remote and has too many logistics issues to be used for a launch shaft. So, the launch shaft would need to be added as part of the Surge Basin, which is undesirable because of all the additional construction activity and access challenges already in play with the Surge Basin and BRPP. The tunneling operation for a tunnel of this length would encompass the entire duration of pumping plant construction, leading to the probable need for an additional working shaft and increasing cost and complexity with competing uses of the site. Furthermore, this scenario would require a maintenance shaft on Victoria Island, which has limited access via two small 90-degree turn bridges on SR 4. At least one of these bridges would have to be replaced at a cost of approximately \$50M.

The Eastern Corridor offers the significant advantage of already having a launch shaft at Lower Roberts Island, within a reasonable tunneling length from the Surge Basin. This launch shaft is currently planned for tunneling to the north, and could be converted to a double-launch shaft for tunneling south to the Surge Basin. The required maintenance shafts on the Jones Tract and Union Island are in favorable locations, and this scenario avoids the addition of a new launch shaft and interference with concurrent work at the Surge Basin and BRPP site. This provided strong rationale for associating the Bethany Reservoir Alignment to the Eastern Corridor.



Twelve locations were initially selected as potential sites for the BRPP and Surge Basin in the area between CCF and Bethany Reservoir, as illustrated in Attachment 2.2.

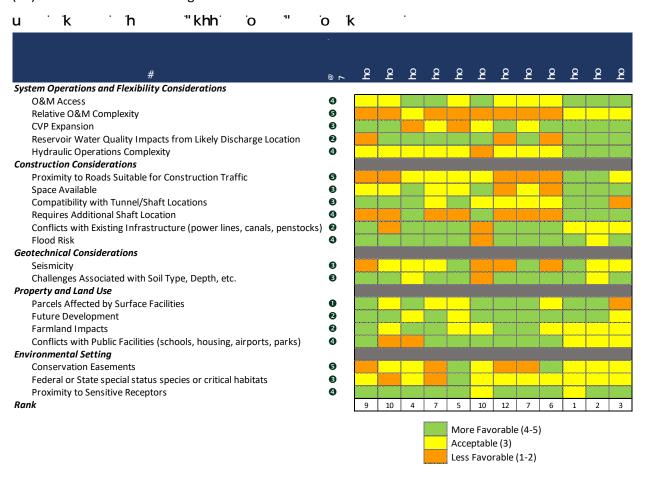
Each of the sites were evaluated considering the following criteria and subcriteria:

- System Operations and Flexibility Considerations Operations and maintenance (O&M) access, relative O&M complexity, CVP expansion, reservoir water quality impacts from likely discharge location, and hydraulic operations complexity
- Construction Considerations Proximity to roads suitable for construction traffic, available space, compatibility with tunnel/shaft locations, conflicts with existing infrastructure (power lines, canals, penstocks, and flood risk
- Geotechnical Considerations Seismicity and challenges associated with soil type, depth, etc.

- Property and Land Use Parcels affected by surface facilities, future development, farmland impacts, and conflicts with public facilities (schools, housing, airports, parks)
- Environmental Setting Conservation easements, federal or state special status species or critical habitats (red-legged frog, kit fox, or other special status species critical habitat, vernal pool habitat, or alkali wetlands), and proximity to sensitive receptors

The sites were ranked using a 1 to 5 scale (4 to 5 being more favorable, 3 being acceptable, 1 to 2 being less favorable) for each of subcriterion. Each one was also assigned an importance factor using a 1 to 5 scale (5 being very important, 1 being of little importance). Each ranking was multiplied by the importance factor to result in an adjusted ranking. A complete listing of subcriteria, importance factors, and ranking factors for each sub-criterion considered for the BRPP and Surge Basin siting study is presented in Attachment 2.3.

The adjusted rankings for each of the sites were summed and then ranked from highest (1) to lowest (12). The results of the rankings are shown in Table 1.



A number of the sites considered for the BRPP and Surge Basin ranked lower within the group due to the following common disadvantages:

- PS-1, PS-4, PS-7, PS-8: Ranked low since these sites would require surface disturbance within conservation easements
- PS-1, PS-2, PS-4, PS-5, PS-7, PS-8, PS-9: Ranked low since these locations would require additional tunnel length and an additional tunnel launch shaft

- PS-1, PS-2, PS-4, PS-5, PS-7, PS-8, PS-9: Ranked low due to significant O&M complexity associated with a cavern-style pumping plant with additional surge chambers and separate Surge Basin sites as would be required for other locations
- PS-6: Ranked low due to challenges with the Surge Basin operating elevations, extensive site
 development requirements, conflicts with high voltage power lines, and difficult access given the
 potential space available
- PS-1, PS-6, PS-7, PS-9: Ranked low due to poor soil conditions and/or proximity to nearby fault crossing and related seismicity challenges
- PS-1, PS-2, PS-7, PS-8, PS-9: Ranked low due to poor location relative to Byron Highway and I-580 and anticipated challenges required to provide site access

The four top-ranking sites (PS-3, PS-10, PS-11, and PS-12) shared the following advantageous characteristics:

- Do not require southern tunnel drive location (compatible with tunnel drive south from Lower Roberts Island)
- Avoids cavern-style pumping plant and separate BRPP and Surge Basin sites
- Adequate room to construct complex without major obstructions and with access to Byron Highway
- Compatible with below grade or partial-below grade Surge Basin
- Compatible with Aqueduct routes that provide a discharge location within Bethany Reservoir that supports circulation within Bethany Reservoir
- Minimal flood risk
- Better ground conditions compared to in-Delta sites

The following points provide details regarding the advantages and disadvantages of the four top ranking sites in addition to those summarized here:

- Site PS-3 ranked fourth-highest within the group. The site advantages include those listed; however, connection with the CVP would require a separate tunnel, and an Aqueduct route to Bethany Reservoir would cross through sensitive vernal pool/conservation areas and highly variable terrain. The site would also only be accessible from Byron Highway, is close to Byron Airport, and potentially conflicts with the future Byron Highway expansion plans.
- Site PS-12 ranked third-highest within the group. This site location would allow for easy connection
 to the CVP and for additional (although indirect) access to the I-580. However, the respective tunnel
 alignment for this site would weave through critical facilities in the area and would potentially
 conflict with the future Byron Highway expansion plans. This site is also somewhat constrained by
 adjacent high-voltage power lines.
- Site PS-11 ranked second-highest within the group. This location would have similar advantages to PS-12; however, it would not likely conflict with future Byron Highway expansion or other future development. Disadvantages would include a lower ground elevation, which would require a partially aboveground Surge Basin and would increase flood risk. In addition, the Aqueduct would require crossing Byron Highway and existing railroad tracks, and the CVP penstocks. Also, the connection to the CVP would be more difficult than for sites PS-10 and PS-12.

Site PS-10 ranked highest within the group. This location would allow for access from both Byron
Highway and the I-580, allow for relatively easy connection to the CVP, and avoid conflict with
future development. In addition, the Aqueduct would not require crossing Byron Highway. One
minor disadvantage identified with this location is that the Aqueduct would require crossing the CVP
penstocks.

Site PS-10 was ultimately selected as the recommended location for the BRPP and Surge Basin, primarily due to its logistical advantages, lack of need for the Aqueduct pipelines to cross the Byron Highway or railroad, proximity to CVP, compatibility with below grade Surge Basin site, and avoidance of conflict with current and potential future infrastructure and development.

o '" k " k " k " k

The Aqueduct portion of the Bethany Reservoir Alignment would convey water from the new BRPP to Bethany Reservoir. The Aqueduct would consist of large-diameter pipelines, pressurized by the pumping plant. The pipelines would be 180-inch-diameter welded steel pipe material. The Aqueduct feeding Bethany Reservoir would include four parallel 180-inch-diameter pipelines.

The Aqueduct would include pipeline appurtenances such as air and vacuum valves and pipelines drains (blowoffs). Most of the Aqueduct would be constructed using open-cut-and-cover methods, including undercrossings at existing roads and canals. However, some portions would be tunneled, as needed, to carry the pipelines under existing surface features. Specifically, the Aqueduct would be tunneled under the existing Jones Pumping Plant discharge penstocks and under existing Bethany Reservoir conservation easements that cannot be avoided by the Aqueduct route.

The Aqueduct feeding Bethany Reservoir would terminate at an outlet structure discharging into Bethany Reservoir (Bethany Reservoir Discharge Structure).

8 '0 ' " ' '

This section covers the siting of the Aqueduct portion of the Bethany Complex and considers Site PS-10 as the starting point in accordance with the siting results for BRPP and Surge Basin portion described in Section 6.

The area between the BRPP and Bethany Reservoir is occupied by multiple canals, the CVP discharge penstocks, high-voltage overhead transmission lines, a high-pressure gas line, a major energy facility, a school, and multiple conservation easements (Attachment 2.1). The terrain is relatively flat and low elevation at the BRPP but becomes more rolling and rises steadily to over elevation 300 feet in areas near Bethany Reservoir. Other than the facilities listed here, most of the land is open space or used for agricultural production.

@ 'h " "

The establishment of potential Aqueduct alignments focused on five primary goals:

The selection always focuses on minimizing alignment length to reduce impacts and cost, but the topography in the Project area is one element that would prevent a short, direct route to Bethany Reservoir. Routes would need to avoid uneven terrain so deep excavations or tunnels could be minimized to the

extent possible. Further, because of the large width of up to four 180-inch-diameter pipes in parallel, relatively wide construction corridors would be needed.

- 2) Existing power lines, canals, gas lines, and other infrastructure would need to be avoided to the extent possible or crossed in favorable locations.
- 4 Consideration would need to be given to following existing roads if feasible, in lieu of new surface disturbance. Where roads would not be followed, it would be good practice to select alignments along the edge of parcels or situated so as not to permanently isolate land that could be used for agriculture or other purposes.
- 4) * Potential wetlands, vernal pools, and other sensitive areas often present major permitting constraints. This route study was not preceded by formal wetland surveys or other means of identifying all potential sensitive areas, but features that could be observed on aerial photos or were known from project records were noted and avoided were possible.
- bordering Bethany Reservoir and other lands to the north (Attachment 2.1) are areas of land that generally cannot be disturbed. Within the overall aqueduct area, there is only one narrow gap in the easements (on Christensen Road). So, alignments would need to pass through that gap, go around the southeastern end of the easements, or be tunneled under the easement(s).

Six optional alignments or routes were identified for the Aqueduct between the BRPP and Bethany Reservoir (Attachment 3.1):

- Alignment A: Generally east-to-west route partially using Christensen Road to pass between conservation easement areas and delivering to the upstream end of the reservoir
- Alignment B: Same as Alignment A, but instead using Kelso Road
- Alignment C: Shorter route through farmed and open space, passing around the southeastern end of the conservation easements and delivering to the downstream end of the reservoir
- Alignment D: Same as Alignment C, but sited to cross the DMC on-grade instead of in a tunnel
- Alignment E: Longer route through farmed and open space and eventually on Mountain House Road, delivering to the downstream end of the reservoir
- Alignment F: Relatively short route through farmed and open space that would tunnel under a narrow strip of easement near the reservoir and discharge to the middle portion of the reservoir

1 10 10

Each alignment was evaluated considering the following criteria and subcriteria:

- Constructability and Cost Overall length, potential utility conflicts and crossings required, general topography (ability to avoid deeper excavations), and geotechnical considerations
- Operational Complexity/Impacts Reservoir water quality benefits/impacts, and O&M considerations
- Property and Land Use Parcels affected by surface facilities, future development, farmland impacts, and conflicts with public facilities (schools, housing, airports, parks), and potential impacts to conservation easements

 Environmental Setting – Federal or state special status species or critical habitats (red-legged frog, kit fox, or other special status species critical habitat, vernal pool habitat, or alkali wetlands), and proximity to sensitive receptors

The alignments were ranked using a 1 to 5 scale (4 and 5 being more favorable, 3 being acceptable, 1 to 2 being less favorable) for each subcriterion. Each criterion was also assigned an importance factor using a 1 to 5 scale (5 being very important, 1 being of little importance). The importance factors were multiplied by the initial ranking to result in an adjusted ranking. A complete listing of subcriteria, importance factors, and ranking factors for each subcriterion considered for the alignment evaluation is presented in Attachment 3.2.

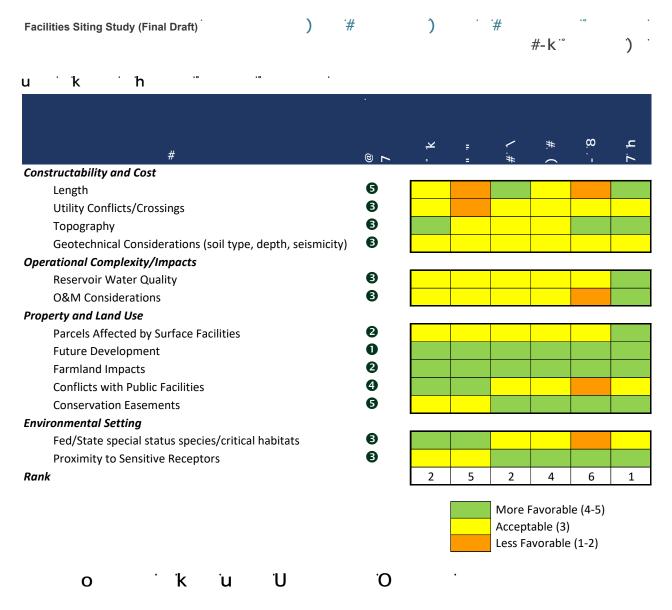
The adjusted rankings for each of the alignments were summed and then ranked from highest (1) to lowest (6). The results of the rankings are shown in Table 2.

Key differentiators that can be observed in Table 2 are as follows:

- Alignment E is considered poor because it would pass in front of Mountain House School and near four to five more private residences than any other alignment.
- There is significant additional route length (approximately 0.5 to 0.75 mile) associated with Alignments B and E.
- Alignment B rates the lowest for utility conflicts because of features along Kelso Road, especially the alignment's proximity to high-voltage overhead transmission line towers.
- Alignments A and B would present challenges to construct more than one pipeline between the
 conservation easements on Christensen Road. The construction corridor for a multiple pipeline
 trench with pipe of this diameter would exceed the space available between conservation
 easements on each side of the road, requiring either significant encroachment and surface
 disturbance of the easements, or tunneling under the easements.
- Alignments A, B, and F would be the most favorable relative to reservoir water quality, with water
 entering at the upper or middle portion of the reservoir. This would offer improved circulation and
 mixing as compared to alignments discharging water at the downstream end.
- Only Alignment F includes room for multiple aqueducts and provides favorable reservoir water
 quality. While Alignments A and B send water to the upstream end of Bethany Reservoir, it does not
 appear that more than one pipeline could be routed down Christensen Road between the
 conservation easements, so these alignments may need to be accompanied by additional pipelines
 on other routes.
- Alignments B, C, and D would have comparatively more challenging topography that could require additional tunneling or more difficult construction conditions.



Alignment F was selected as the recommended route for the Aqueduct due to its generally shorter length, minimal effects on reservoir water quality, favorable topography, and reasonable distance from sensitive receptors. Further, it would have no impact on the conservation easements or major construction constraints imposed by the easements (assuming tunneling far beneath the easements is deemed acceptable by the easements' controlling interests).



Construction of many Project facilities would occur in locations served by roads that currently are characterized by traffic congestion and/or poor road conditions. Some of the roads are located on top of levees that have some foundation problems. Therefore, construction of Project features would require improvement of some roads, new access roads, and new interchanges. Existing roadways that possibly could be used to access construction sites were analyzed as part of the Project.

- '= '#

The Surface Transportation Assistance Act (STAA) of 1982 allows large trucks to operate on the Interstate and certain primary routes. These routes are referred to as the National Network. These trucks, referred to as STAA trucks, are longer than trucks identified as "California legal trucks." On STAA routes the maximum length of trailer of a semitrailer truck is 53 feet, and STAA trucks have a larger turning radius than most local roads can accommodate. STAA Terminal Access routes are roads where STAA trucks may exit the interstate and travel onto State and local routes. Considering road systems could be used during Project construction, Interstate 5, Interstate 580 and Interstate 205 near Tracy are National STAA truck routes. State Route 12, portions of State Route 4 between Interstate 5 and the Port of Stockton, and portions of State Route 160 between State Route 4 and a location south of Isleton are STAA Terminal Access routes.

California Legal Truck Routes provide a network for large California Legal Trucks to operate. California Legal Trucks must meet certain requirements, including a maximum length of 65 feet for single trailers and trailers with 40-feet dimension from kingpin to rear axle (KPRA) and 75 feet for double trailers. Geometric conditions of the roads, including the presence of a sharp turning radius, are used to classify roads as California Legal with KPRA Advisory routes. State Route 160 between Isleton and a location on Sutter Island (0.8 miles south of Courtland) and State Route 4 between Tracy Boulevard in San Joaquin County to Sand Creek Road in the City of Brentwood are identified as a California Legal Truck Route with a KPRA Advisory.

State Route 160 between a location 1 mile north of the Freeport Bridge and a location on Sutter Island (0.8 miles south of Courtland), State Route 4 between the Port of Stockton and Tracy Boulevard in San Joaquin County, and State Route 4 between Sand Creek Road in City of Brentwood and State Route 160 are identified as a California Legal Truck Route for 65-foot maximum length trailers with 40-foot KPRA.

Interstates 5, 580 and 205 are in good condition and characterized by periods of traffic congestion.

State Routes 4 and 12 are generally in good condition based upon limited pavement condition data and characterized by periods of traffic congestion. State Routes 4 and 12 in these reaches include several bridges including multiple moveable bridges. Intermittent traffic delays occur due to bridge openings related to navigation needs.

State Route 4 in these reaches include three bridges. The bridges across Old River and Middle River are characterized by narrow lanes and sharp turns on the approach roadway consistent with its designation as an advisory truck route due to reduced lane width and the acute angle of approach. On State Route 12, two drawbridges across the Mokelumne River and Little Potato Slough are moveable bridges that are characterized by intermittent traffic delays.

State Route 160 is primarily constructed on top of Sacramento River levees and provides access to communities along the Sacramento River. This route has advisory truck limits on the length of trucks allowed along this road that is characterized by reaches without adequate shoulders. State Route 160 in this reach includes four bridges which are all moveable bridges.

More than thirty local roads could provide direct access to potential Project construction sites in the Delta. Many of these roads are characterized as rural two-lane paved roadways with 10-foot wide lanes and minimal shoulders. These roads are used by local and agricultural vehicles and traffic. These roads include Hood-Franklin Road, Twin Cities Road, West Walnut Grove Road, West Eight Mile Road, West March Lane, West Byron Road, Mountain House Parkway, and Tracy Boulevard, and are summarized in Table 3.

| u o | K # | | | | | |
|------------|-----------------------|-------|----|-----|-----|---------------------------------|
| | | | | 0 · | o . | |
| # . | k · | u · | Ο. | • | • | О . |
| Sacramento | Hood-Franklin Road | paved | 2 | 12 | 2 | Interstate 5 to State Route 160 |
| Sacramento | Lambert Road | paved | 2 | 10 | 1 | Interstate 5 to State Route 160 |

|) | · # |) | · ·# | •0 | • |
|---|------------|---|------|-------------------|-----|
| | | | | #-k ° |) . |

| | | | | 0 . | o ‡ | |
|-------------|------------------------|--------|----|-----|--------|---|
| # . | k · | u · | Ο. | | | 0 |
| Sacramento | Dierssen Road | gravel | 2 | 9 | 0 | Franklin Boulevard to 1.4 miles west of Interstate 5 |
| Sacramento | Twin Cities Road | paved | 2 | 12 | 1 | Interstate 5 to River Road |
| Sacramento | Franklin Blvd | paved | 2 | 10 | 2 to 4 | Lambert Road to Twin Cities Blvd |
| Sacramento | Russell Road | paved | 2 | 10 | 0 to 1 | River Road to Herzog Road |
| Sacramento | Vorden Road | paved | 2 | 10 | 0 to 1 | River Road to Herzog Road |
| Sacramento | Herzog Road | paved | 2 | 10 | 0 to 1 | Vorden Road to Lambert Road |
| Sacramento | Jackson Slough Road | paved | 2 | 10 | 0 to 1 | State Route 160 to State Route 12 |
| Sacramento | Terminous Road | paved | 2 | 10 | 0 to 1 | Jackson Slough Road to State Route 12 |
| San Joaquin | W Walnut Grove Road | paved | 2 | 12 | 4 | Interstate 5 to River Road |
| San Joaquin | Lauffer Road | gravel | 2 | 10 | 0 | Vail Road to Mokelumne River |
| San Joaquin | Vail Road | paved | 2 | 10 | 0 to 1 | W. Walnut Grove Road to Mokelumne River |
| San Joaquin | Blossom Road | paved | 2 | 10 | 0 to 1 | Peltier Road to W Walnut Grove Blvd |
| San Joaquin | Staten Island Road | paved | 2 | 10 | 1 | W. Walnut Grove Road to S Fork Mokelumne River |
| San Joaquin | Gas Well Road | gravel | 2 | 8 | 0 | Staten Island Road to S Fork Mokelumne River |
| San Joaquin | Gotta Road | paved | 2 | 10 | 0 to 1 | N. Jacob Brack Road to N Guard Road |
| San Joaquin | N Jacob Brack Road | paved | 2 | 10 | 0 to 1 | Turner Road/Interstate 5 interchange to Gotta Road |
| San Joaquin | N Guard Road | paved | 2 | 10 | 0 to 1 | State Route 12 to Gotta Road |
| San Joaquin | Stefani Road | paved | 2 | 8 | 0 | W 8 Mile Road to Telephone Cut |
| San Joaquin | Glasscock Road | paved | 2 | 10 | 0 to 1 | State Route 12 to south of Sycamore Slough |
| San Joaquin | Correia Road | paved | 2 | 10 | 0 to 1 | State Route 12 to Potato Road at White Slough |
| San Joaquin | Peltier Road | paved | 2 | 10 | 0 to 1 | Interstate 5 to Blossom Road |
| San Joaquin | W Eight Mile Road | paved | 2 | 10 | 0 to 1 | Interstate 5 to Empire Tract Road at Little Connection Slough |

| | | | | Ο. | О . | |
|--------------|------------------------|--------|--------|-----|--------|---|
| | | | | ‡ . | ‡ . | |
| # . | k · | u · | 0 . | • | • | О . |
| San Joaquin | W March Ln | paved | 6 | 12 | 0 | Interstate 5 to March Ln |
| San Joaquin | Holt Road | paved | 2 | 10 | 0 to 1 | State Route 4 to San Joaquin River |
| San Joaquin | Jacobs Road | paved | 2 | 10 | 0 to 1 | Holt Road to Burns Cutoff Road |
| San Joaquin | Inland Dr | paved | 2 | 10 | 0 to 1 | State Route 4 to House Road at Burns Cut |
| San Joaquin | Bacon Island Road | paved | 2 | 10 | 0 to 2 | State Route 4 to S. Bacon Island Road Bridge at Middle River |
| San Joaquin | S Bacon Island Road | paved | 2 | 10 | 0 to 2 | S. Bacon Island Road Bridge at Middle River to Connection Slough Swing Bridge |
| San Joaquin | Lower Jones Road | paved | 2 | 10 | 0 to 1 | Holt Road to W Lower Jones Road |
| San Joaquin | W Lower Jones Road | gravel | 2 | 8 | 0 | Lower Jones Road to Bacon Island Road |
| San Joaquin | McDonald Road | paved | 2 | 10 | 0 to 1 | Inland Dr to Whiskey Slough |
| San Joaquin | Tracy Blvd | paved | 2 | 12 | 0 to 4 | State Route 4 to Interstate 205 |
| San Joaquin | Mountain House Pkwy | paved | 4 to 6 | 12 | 4 | Interstate 205 to Byron Road |
| San Joaquin | Byron Road | paved | 2 | 12 | 2 | Mountain House Pkwy to State Route 4 |
| San Joaquin | Clifton Court Road | paved | 2 | 10 | 0 | Tracy Blvd to Bonetti Road |
| San Joaquin | Bonetti Road | paved | 2 | 9 | 0 | North of Clifton Court Road |
| Contra Costa | Byron Highway | paved | 2 | 12 | 2 to 4 | Mountain House Pkwy to State Route 4 |
| Alameda | Byron Bethany Road | paved | 2 | 12 | 2 to 4 | Mountain House Pkwy to State Route 4 |
| Alameda | W. Grant Line Road | paved | 2 | 12 | 1 to 4 | Interstate 580 to Great Valley Pkwy |
| Alameda | Kelso Road | paved | 2 | 11 | 1 | Great Valley Pkwy to Mountain House Road |
| Alameda | Mountain House Road | paved | 2 | 12 | 1 to 2 | W. Grant Line Road to Byron Bethany Road |

Overall conditions and pavement conditions on existing roads that could provide direct access to potential Project construction sites range from poor to good. However, most roads that could provide direct access to potential construction sites are poor or fair.

There are more than 40 bridges, including 12 moveable bridges, along local roads that could provide direct access to potential Project construction sites. Caltrans has rated 14 of these local bridges as

functionally obsolete or structurally deficient. Seven local bridges are being planned in the area being considered for potential Project construction sites, including:

- Bridge along Twin Cities Road across Snodgrass Slough was identified as Functionally Obsolete, and
 is planned to be replaced by a new structure on a different alignment. Sacramento County has
 completed environmental review and is in the process of final design and right of way acquisition.
- Bridge along Walnut Grove Road across Mokelumne River is a swing bridge was identified as Structurally Deficient, and identified on the Highway Bridge Program to be replaced.
- Bridge along the Walnut Grove crossing of the Sacramento River was identified as Structurally Deficient, and identified on the Highway Bridge Program to be replaced or rehabilitated.
- Bridge along Franklin Boulevard across the Mokelumne River Overflow was identified as Structurally Deficient, and identified on the Highway Bridge Program to be replaced.
- Bridge along Eight Mile Road across White Slough (Honker Cut) was identified as Functionally Obsolete, and identified on the Highway Bridge Program to be replaced.
- Bridge along Byron Highway across the California Aqueduct was identified as Structurally Deficient. Contra Costa County has initiated an environmental review process to replace the bridge.
- Bridge along Cotta Road across Upland Canal was identified as Structurally Deficient, and identified on the Highway Bridge Program to be replaced.
- Culvert on Mountain House Road at Byron Bethany Irrigation District Canal is believed to be rated deficient. The portion of Mountain House Road between W. Grant Line Road and Kelso Road is signed at 7 Ton Maximum Load.

The timing of potential bridge retrofits or replacements is not currently known. Woodward Island Bridge connecting Upper Jones Tract at Bacon Island Road with Woodward Island over Middle River was constructed by San Joaquin County in 2019 to replace the Woodward Island Ferry. However, this bridge was only designed for local residents, employees, and agricultural traffic.



Most of the existing local roadways are characterized by poor pavement or foundation conditions, narrow paved areas with small or no shoulders, bridges with poor conditions or narrow lanes, and/or roads and bridges with traffic congestion. Therefore, a series of transportation projects would be considered to access the Project construction sites. The potential roadway projects could include:

- Parallel access or haul roads to provide construction and operations access to avoid using levee roads.
- Expansion of existing roads to provide wider paved areas, including wider shoulders.
- Realignment of roads to accommodate new interchanges or rail-served material depots.
- New access interchanges.
- New haul road to Bethany Reservoir to support construction traffic.
- Bridge modifications.
- Park-and-Ride Centers or Materials Depots to provide a central location for employees and materials to transfer from numerous employee vehicles or small trucks to buses and larger trucks.
- Asphalt overlays for existing roads both during and following construction.

Selection of the roadways used for construction are summarized in the CER Appendix E1 *Logistics Strategy* and were be based upon other uses of the roads by the communities, including proximity to communities, schools, emergency responders, wildlife areas, and recreation areas; and use of the roadways as major commute corridors (e.g., State Routes 4 and 12). Roadway modifications were selected to minimize the miles traveled by construction equipment and employees. Roadways would be upgraded to the standards of the agency that owns the roadways, with thoughts around how the roadways are now utilized, and the potential for the work to provide other benefits such as widened shoulders for increased bicycle use.

The selection of the route for the new haul road to Bethany Reservoir was analyzed separately and is described in additional detail below.

Park-and-ride areas would be provided to convey the employees to the construction sites on electric buses or vans (recharged by on-site solar panels, when possible) to reduce traffic congestion and air quality emissions. Two park and ride facilities, one at Interstate 5 and Hood-Franklin Road and one near Interstate 5 at Charter Way in Stockton were identified for the consolidation centers (CER Appendix E1).

The Bethany Reservoir haul route alignment initially considered during concept design follows an existing unpaved patrol and access road leading from Mountain House Road along the northern side of the SWP canal system and up the hillside leading to Bethany Reservoir. The terrain in this area is steep and variable. The existing access road generally follows topography, resulting in grades that exceed the maximum requirements for the Bethany Reservoir Alignment haul route of 7 percent, based on California Department of Transportation (Caltrans) maximum grades for trucks in rural areas. Additionally, the existing access road would need to be widened to support two-way construction traffic.

Modifications to upgrade the existing access road for the Bethany Reservoir Alignment were found to impact areas of alkali wetland, and resulted in significant quantities of cut and fill, which expanded the temporary and permanent footprint of the haul route. Consequently, several alternative access road alignments were considered to minimize wetland impacts while optimizing the cut and fill requirements for construction. These alternatives are illustrated in Attachment 4 - Bethany Reservoir Haul Route Alignment Study. The plan view contained therein shows each of the alternative alignments, with associated profiles indicating grades and locations of sections of cut and fill. The characteristics of each alternative are summarized in Table 4 for comparative purposes only.

| u "# k " | • | | | |
|--|---------|---------|---------|--------|
| M # | @ 'k ' | • | • • • | • • • |
| Length ^[a] (miles) | 1.1 | 1.1 | 1.0 | 1.2 |
| Max grade ^[b] (percent) | 7 | 7 | 7 | 7 |
| Existing Disturbance (acres) | 2.7 | 1.6 | 2.7 | 0.6 |
| Total Disturbance Footprint ^[c] (acres) | 9.7 | 11.4 | 11.6 | 9.5 |
| Net Increase in Disturbance (acres) | 7.0 | 9.8 | 8.9 | 8.9 |
| Cut volume ^[d] (CY) | 153,000 | 196,000 | 197,000 | 64,000 |
| Fill volumed (CY) | 1,100 | 28,000 | 32,000 | 19,000 |

| M # | @ 'k ' | • | • • • | • |
|---|-------------|-------------|-------------|------------|
| Earthworks Balance ^[e] (CY) | 151,900 cut | 168,000 cut | 165,000 cut | 45,000 cut |
| Area of encroachment into wetlands (SF) | 24,000 | 8,000 | None | None |

[[]a] Concept design is based on mapping contours in the absence of detailed site survey.

Notes:

CY = cubic yard(s)

SF = square foot (feet)

-

Each considered haul route would achieve the required grades, but with varying lengths, cut and fill quantities, and wetland impacts as summarized in Table 4. Attachment 4 shows the locations of the cut and fill areas. The attributes of the evaluated haul routes can be summarized as follows:

- Initial Route: Follows an existing access track running along the southern edge of the alkali wetlands. The route crosses the wetlands at three separate locations, yielding the largest wetland impacts of 24,000 square feet. The alignment follows natural ground and is relatively flat for approximately the first half of its length, with the second half common with Alternative 1. Large cuts would be required to minimize the steep road slope in the second half, but still would not achieve 7 percent grades. As a result of following natural ground initially, the concept design has a lower surplus cut earthworks balance than Alternative 1.
- Alternative 1: Runs parallel to the existing SWP canal and would involve significant cut earthworks to achieve feasible grades. This route is also near two large transmission towers (that is, within approximately 20 feet), so foundation conditions for these towers would need to be considered. The route is also in direct conflict with a couple of low voltage powerline poles. This route is close to the base of natural slopes and fill slopes supporting the California Aqueduct, so earthwork in this area would need to consider potential impacts to the SWP system. This route encroaches into the identified alkali wetlands at two locations, resulting in a net impact of 8,000 square feet. The second half of Alternative 1 alignment is common with the Initial Route.
- Alternative 2: Exits from Mountain House Road at a point further north than the Initial Route or
 Alternative 1 and avoids wetland impacts. The route runs close to existing access roads that are used
 for electrical tower and power pole maintenance. However, this access route is oriented over a hill
 that requires significant volumes of cut earthwork to achieve feasible grades.
- Alternative 3: Exits from Mountain House Road at a point further north than all other consider routes. The haul route generally follows natural contours of the topography to minimize cut and fill requirements but results in a slightly longer overall alignment. This alternative has the least amount of cut and fill, the smallest disturbance footprint, and has no impact on wetlands.

[[]b] Caltrans maximum grade for trucks of 7% on rural areas has been adopted

[[]c] Earthwork concept design is based on 2H:1V cut & fill slopes

^[d] No allowance for topsoil stripping or reinstatement, unsuitable materials, or flattening batters for stabilization in areas of weak or highly erodible material.

[[]e] Earthworks volumes are excess quantities and are quantified as solid in-place ("bank") volumes and ignore considerations such as bulking factors, cut to fill losses, etc.



Based on this evaluation, Alternative 3 is considered the most feasible from an engineering perspective and is recommended as the preferred alternative for the Bethany Reservoir haul route. Given the grade and anticipated construction traffic loading, the road would be paved in accordance with adopted Project standards.

o ko U) O

Railroads were considered to be used to deliver tunnel liner segments to tunnel launch shafts. The two railroad companies in the Project area include the Union Pacific Railroad (UPRR) and Burlington Northern Santa Fe Railroad (BNSF). Use of railroads would require construction of a rail-served material depot with rail sidings. The rail siding would be designed to allow for the train to leave or pick-up rail cars, hold the rail cars, and off-load or load the rail cars. The depot would include areas where trains would move off the main line to deposit the rail cars and areas to transfer the materials to trucks.

- k V ')

In general, rail facilities are designed and constructed to handle either unit train service (full train loads at one time) or manifest service (less than a full train load at one time). Unit trains are typically in the 100-car size with all cars containing the same commodity originating from the same location to specific destination points with stops only to allow changes of railroad crews. Manifest trains are defined by the movement of various commodities from a wide range of origins and to a wide range of destinations. Most rail cars moving from an origin facility to a destination move via manifest train service. Both unit trains and manifest trains handle multiple types of rail cars.

Railroads typically own and maintain the rights-of-way (ROW) for the rail lines. Railroads maintain the railroad ROW and rail infrastructure. Railroads may elect to allow public agencies to operate passenger or commuter service upon these lines, such as Amtrak or Altamont Corridor Express (ACE). However, the public agencies hold no property rights on the rail lines, although the public agencies could participate in supporting upgrades and maintenance. Dispatch of all rail movements, including passenger and freight trains, are controlled by the railroad companies.

UPRR owns the Sacramento-Lathrop and Lathrop-Byron rail lines. The Sacramento-Lathrop rail line is a general freight line that extends from Sacramento through Stockton (part of the UPRR Sacramento Subdivision) and from Stockton to Lathrop (part of the UPRR Fresno Subdivision) along an alignment generally parallel to Interstate 5. This line is capable of handling rail cars of any weight and/or size. Currently, only freight trains operate between Sacramento and Stockton. The San Joaquin Regional Rail Commission, operators of the ACE, has recently announced its desire to seek permission from UPRR to operate commuter train service between Stockton and Sacramento.

UPRR also owns the Lathrop — Byron rail line that extends from Lathrop moving southwesterly into Tracy and then northwesterly through the communities of Mountain House, Byron, and Brentwood as part of the UPRR Tracy Subdivision. This line once served as a major freight corridor for rail traffic to serve the San Francisco Bay Area. Currently UPRR only operates local freight service between the Stockton and rail yards to serve industrial customers. The rail line from downtown Tracy and through the communities of Mountain House, Byron, and Brentwood has not been used since the early 1990s and only provides rail car storage. The line is maintained to a level suitable for slow rail movements of empty rail cars.

| Facilities Siting Study (Final Draft) |) | · # |) | · ·# | • 0 | |
|---------------------------------------|---|------------|---|------|-----------------|---|
| | | | | | #-k |) |

BNSF owns the Antioch - Stockton rail line that extends from Antioch to Stockton as part of the BNSF Stockton Subdivision. This line serves as the BNSF primary freight corridor serving the San Francisco Bay Area, including movement of premium intermodal and automobile trains. Amtrak operates over this line with the "San Joaquins" passenger trains seven times per weekday in each direction (fourteen total trains). The line is capable of handling rail cars of any weight and/or size.

h ko U) O

Rail-Served Materials Depots for the Project were identified related to proximity to tunnel launch shaft sites to provide tunnel liner segments, TBM equipment, and aggregate to the construction sites. A track facility with connection to a mainline would be utilized for the storing, sorting, loading and unloading of rail cars for one or more industries. The layout of the track facility would be related to use of the facilities by unit trains or manifest trains. Since proximity to rail is poor at most sites, and good freeway access exists, only one Rail-Served Materials Depots was selected for further consideration, as summarized below:

• Extended from either UPRR or the BNSF, rail lines that are located on the Port of Stockton and would be extend with a Project-rail line onto Lower Roberts Island to deliver materials near the RTM management area where the materials would be transferred to trucks for delivery to the tunnel launch shaft site.

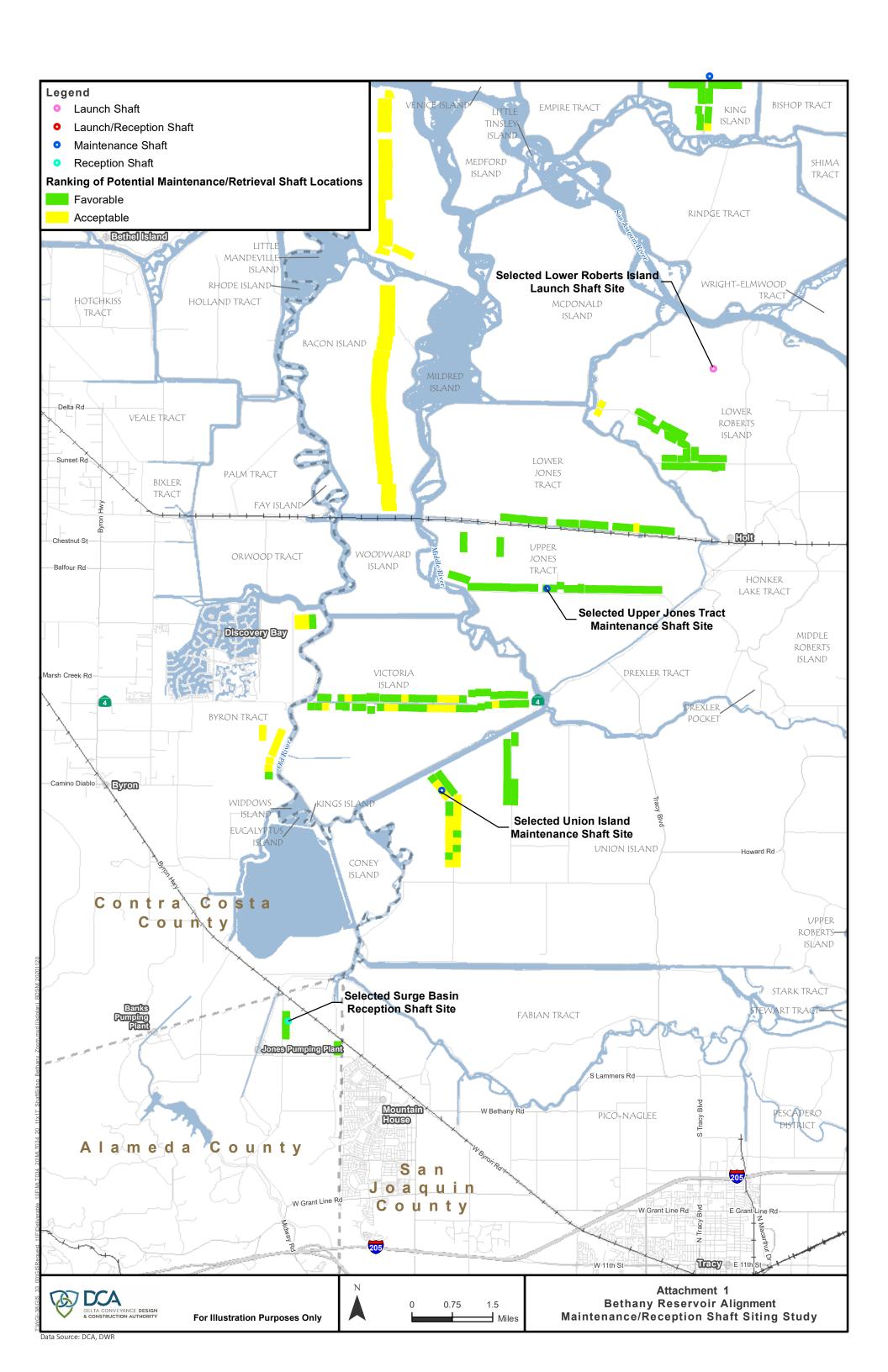
k .

California Department of Water Resources (DWR). 2023. *Delta Conveyance Project Final Environmental Impact Report*. SCH# 2020010227. December 2023.

Delta Conveyance Design and Construction Authority (DCA). 2022. Delta Conveyance Final Draft Engineering Project Report. Bethany Reservoir Alternative. May 2022.

Delta Conveyance Design and Construction Authority (DCA). 2023. Delta Conveyance Final Draft Engineering Project Report Update Bethany Reservoir Alternative. November 2023.

U k o o o

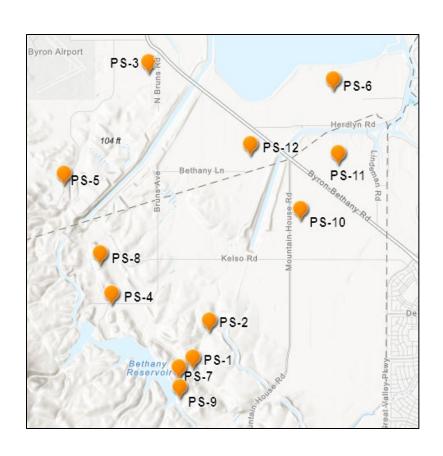


" k h h ...
o "o o



Attathasem 2.1

General Area for Siting of the Bethany Reservoir Pumping Plant and Surge Basin



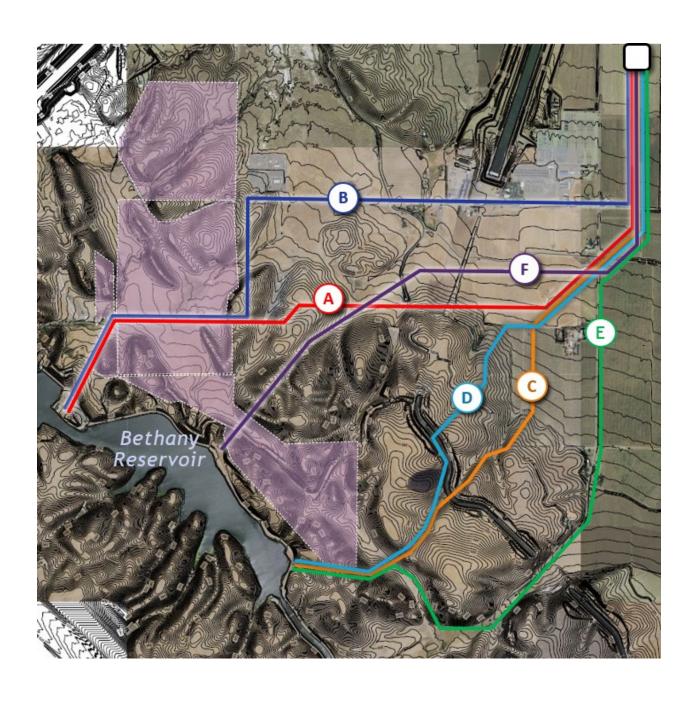
Attachment 2.2

Potential Site Locations for the Bethany Reservoir Pumping Plant and Surge Basin Site

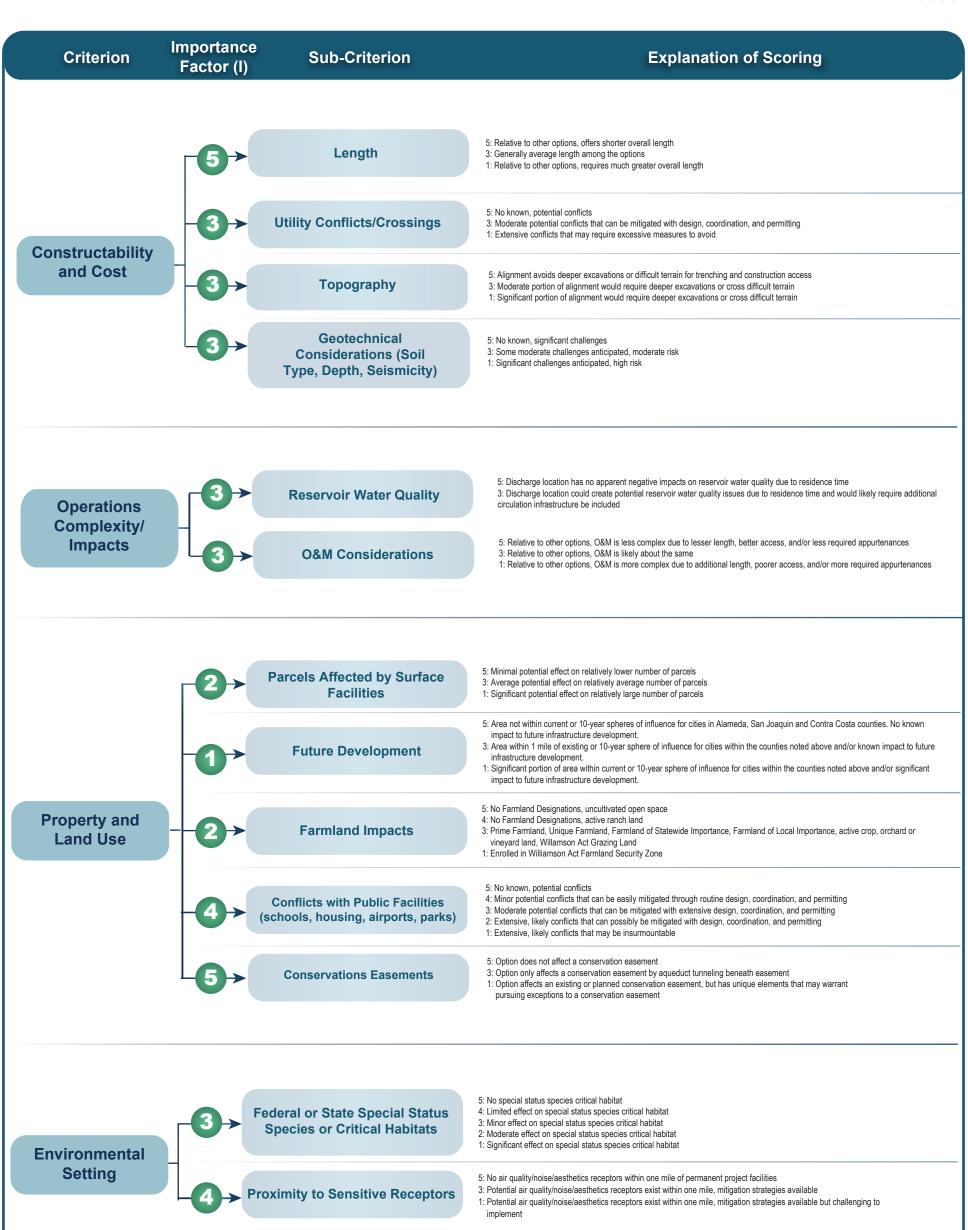
Importance Criterion **Sub-Criterion Explanation of Scoring** Factor (I) 5: Excellent access for O&M vehicles and equipment on high ranking roads over short distances 4: Good O&M access on moderately ranked roads and reasonably short distances 3: Acceptable O&M access with potential speed or load restrictions or tight turning radii over moderate distance **O&M Access** 2: Same as 3, except over long distance 1: Challenging O&M access requiring very slow speed over very long distance 5: Relative to other alternatives, O&M is less complex, requires routine equipment and skills similar to other nearby facilities (i.e. surface pumping plant with relatively short penstocks) **Relative O&M Complexity** 3: Relative to other alternatives, O&M is of average complexity, requires some specialized equipment and skills (i.e. long penstocks w/ cathodic protection systems) 1: Relative to other alternatives, more complex O&M requirements with higher risk of failure (i.e. deep cavern pumping plant) **System Operations** 5: Close proximity to DMC with minimal to no crossings **CVP Expansion** 3: Practical route to DMC with moderate length and crossings and Flexibility 1: Significant length and crossings to connect to DMC **Considerations Reservoir Water Quality Impacts** 4: Likely discharge location has no apparent negative impacts on water quality due to residence time 2: Likely discharge location could create potential water quality issues due to residence time and would likely require additional from Likely Discharge Location circulation infrastructure be included 5: Location and configuration of pumping plant provides relatively straight forward solution to handling of surge flows/pressures. **Hydraulic Operations** 3: Location and configuration of pumping plant requires more complex solution to handling of surge flows/pressures. Complexity 1: Location and configuration of pumping plant requires potentially excessive solution to handling of surge flows/pressures. 5: Ability to connect to I-580 and Byron Hwy with moderate construction effort (i.e. construction of new interchange, new roads, etc.) **Proximity to Roads Suitable** 3: Ability to connect to only Byron Hwy and/or lower capacity roads with moderate construction efforts and/or improvements to existing roads (i.e. construction of new interchange, new roads, etc.) for Construction Traffic 1: Challenging construction access requiring use of low capacity roads and multiple new roads, bridges and/or complex infrastructure 5: Construction footprint for project facilities easily fits within proposed site 3: Construction footprint fits proposed site with moderate means/methods restrictions Space Available 1: Construction footprint may fit proposed site by using extensive earthwork, moving adjacent infrastructure, and/or securing special permits and clearances Construction 5: Tunnel corridor avoids crossing critical infrastructure and results in overall total shorter alignment; shafts are accessible **Considerations** 4: Tunnel corridor requires increased overall alignment length to avoid crossing critical infrastructure; shafts are accessible **Compatibility with Tunnel** 3: Tunnel corridor crosses near critical infrastructure, but can be managed/minimized; shafts are accessible **Shaft Locations** 2: Tunnel corridor requires complex alignment to avoid crossing critical infrastructure; shafts are accessible 1: Tunnel corridor crosses critical infrastructure; shaft in congested location and difficult to access **Requires Additional Shaft** 5: Does not require an additional tunnel launch shaft in the South Delta area due to overall tunnel length and changing ground conditions 1: Does require an additional tunnel launch shaft in the South Delta area due to overall tunnel length and changing ground conditions Location 5: No known, potential conflicts **Conflicts with Existing** 4: Minor potential conflicts that can be easily mitigated thru routine design, coordination, and permitting Infrastructure (power lines, 3: Moderate potential conflicts that can be mitigated with extensive design, coordination, and permitting 2: Extensive likely conflicts that can possibly be mitigated with design, coordination, and permitting canals, penstocks) 1: Extensive conflicts that may take excessive effort to avoid 5: Topography is more than 3 feet above El. 20.8 ft (Est. 200-yr flood elevation w/ future Sea-Level Rise and Climate Change hydrology for Year 2100) Flood Risk 3: Topography is between 0 and 3 feet above El. 20.8 ft (Est. 200-yr flood elevation w/ future Sea-Level Rise and Climate Change 1: Topography is below El. 20.8 ft (Est. 200-yr flood elevation w/ future Sea-Level Rise and Climate Change hydrology for Year 2100) 5: No known nearby faults (beyond 1 mile from site) 3: Known nearby fault crossing, possible moderate challenges anticipated (0.25 to 1 mile from site) Seismicity 1: Known nearby fault crossing, significant challenges anticipated (less than 0.25 mile from site) **Geotechnical** 5: No known, significant challenges **Considerations** 4: Few minor challenges anticipated, low risk **Challenges Associated with** 3: Few moderate challenges anticipated, moderate risk Soil Type, Depth, etc. 2: Several moderate challenges anticipated, moderate risk 1: Significant challenges anticipated, high risk 5: Minimal potential effect on relatively lower number of parcels Parcels Affected by Surface 3: Average potential effect on relatively average number of parcels 1: Significant potential effect on relatively large number of parcels **Facilities** 5: Area not within current or 10-year spheres of influence for cities in Alameda, San Joaquin and Contra Costa counties. No known impact to future infrastructure development. 3: Area within 1 mile of existing or 10-year sphere of influence for cities within the counties noted above and/or known impact to future **Future Development** infrastructure development. 1: Significant portion of area within current or 10-year sphere of influence for cities within the counties noted above and/or significant **Property and** impact to future infrastructure development. **Land Use** 5: No Farmland Designations, uncultivated open space 4: No Farmland Designations, active ranch land **Farmland Impacts** 3: Prime Farmland, Unique Farmland, Farmland of Statewide Importance, Farmland of Local Importance, active crop, orchard or vineyard land, Willamson Act Grazing Land 1: Enrolled in Williamson Act Farmland Security Zone 5: No known, potential conflicts 4: Minor potential conflicts that can be easily mitigated through routine design, coordination, and permitting **Conflicts with Public Facilities** 3: Moderate potential conflicts that can be mitigated with extensive design, coordination, and per (schools, housing, airports, parks) 2: Extensive, likely conflicts that can possibly be mitigated with design, coordination, and permitting 1: Extensive, likely conflicts that may be insurmountable 5: Option does not affect a conservation easement 3: Option only affects a conservation easement by aqueduct tunneling beneath easement **Conservation Easements** 1: Option affects an existing or planned conservation easement, but has unique elements that may warrant pursuing exceptions to a conservation easement 5: No special status species critical habitat 4: Limited effect on special status species critical habitat **Environmental Federal or State Special Status** 3: Minor effect on special status species critical habitat **Species or Critical Habitats** Setting 2: Moderate effect on special status species critical habitat 1: Significant effect on special status species critical habitat 5: No air quality/noise/aesthetics receptors within one mile of permanent project facilities 3: Potential air quality/noise/aesthetics receptors exist within one mile, mitigation strategies available **Proximity to Sensitive Receptors** 1: Potential air quality/noise/aesthetics receptors exist within one mile, mitigation strategies available but challenging to



Attachment 2.3 BRPP and Surge Basin Siting Criteria " k " " o o

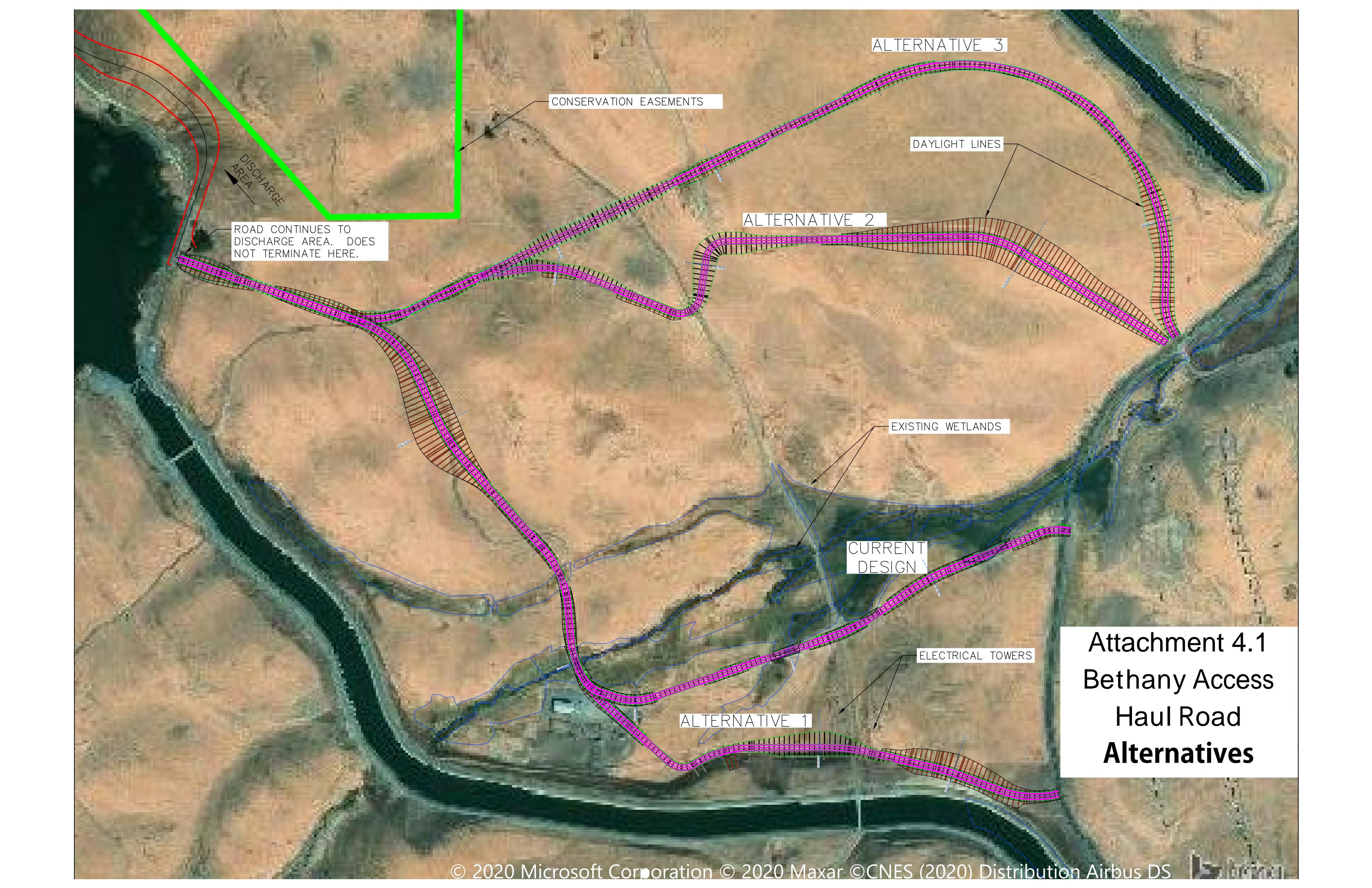


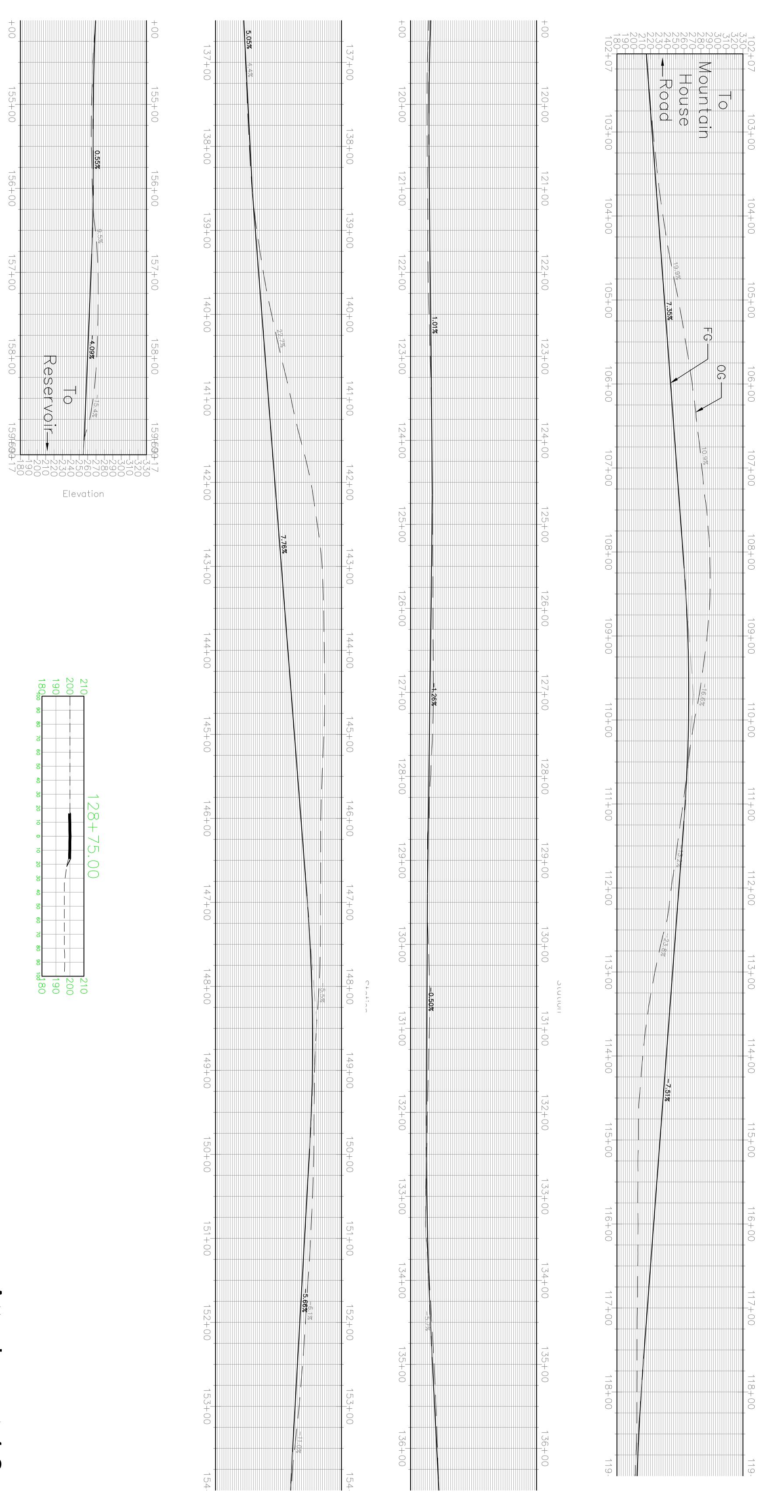
Attachment 3.1
Optional Aqueduct Alignments

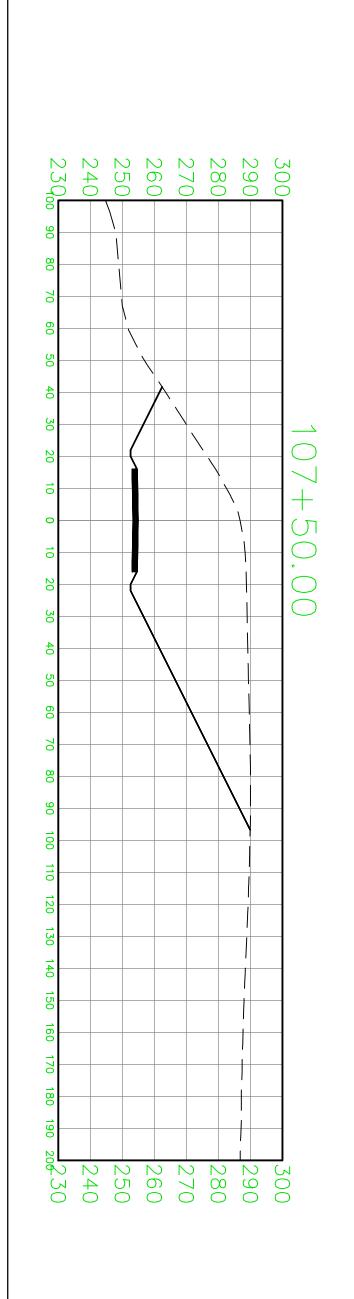




" k = k " o







+00

155+00

156+00

157+00

158+00

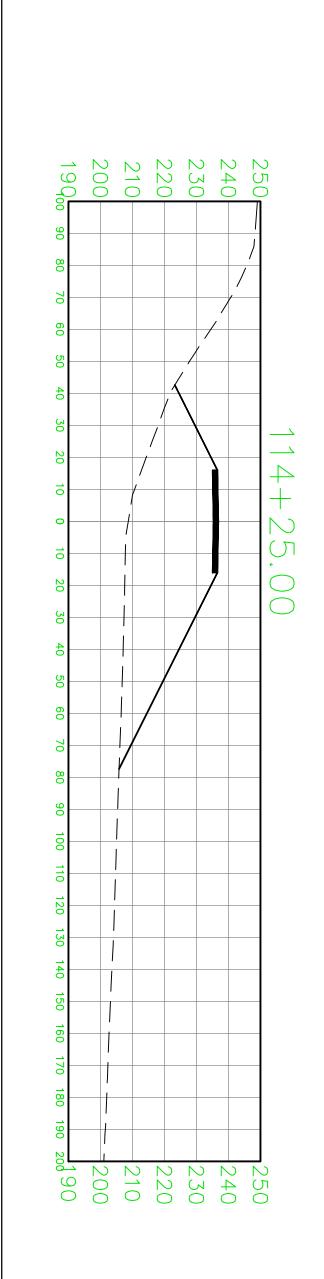
Rese

0

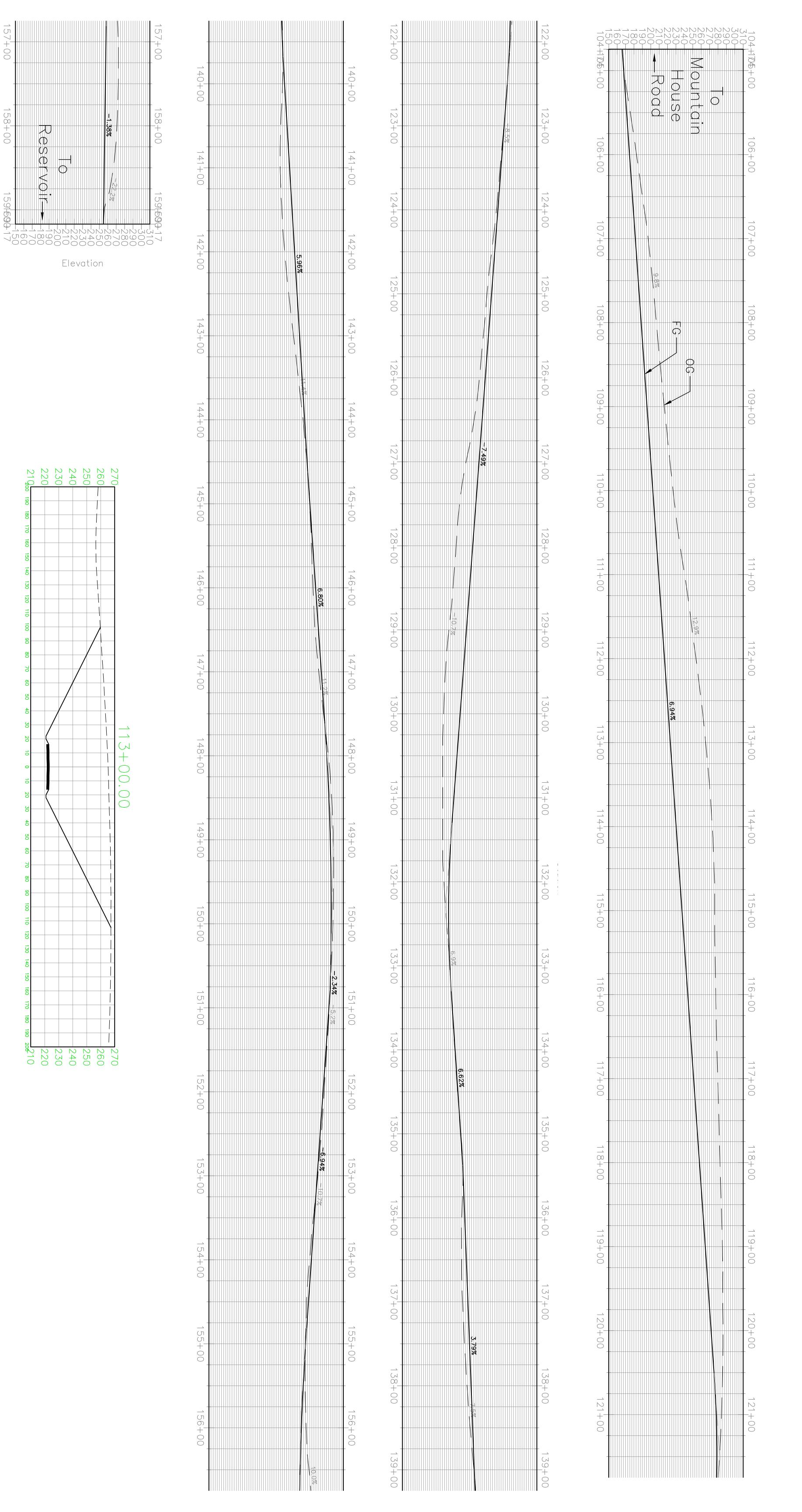
Elevation

210 200 190 180

 \bigcirc



Attachment 4.2 Bethany Haul Access Road ALT 1

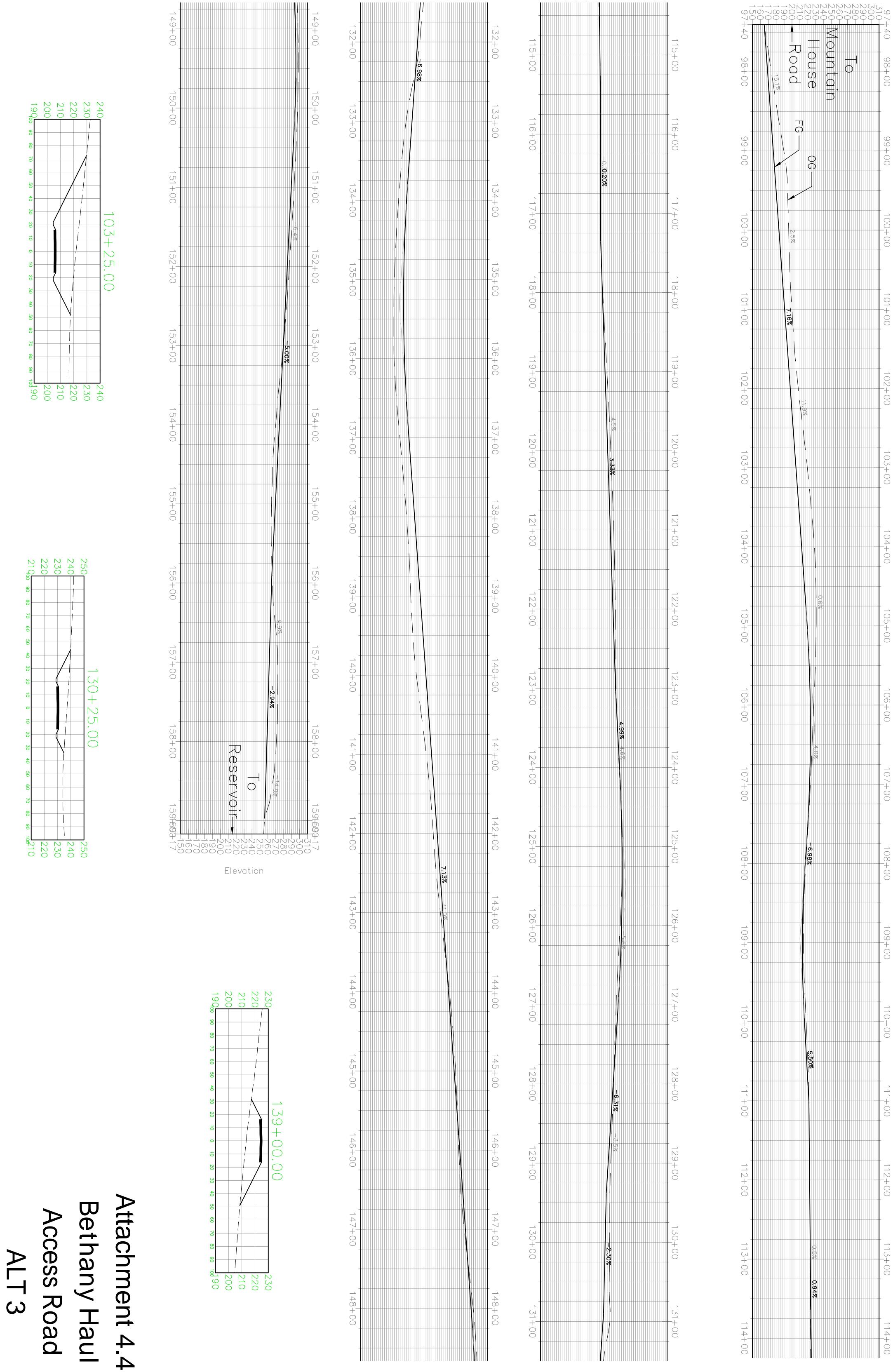


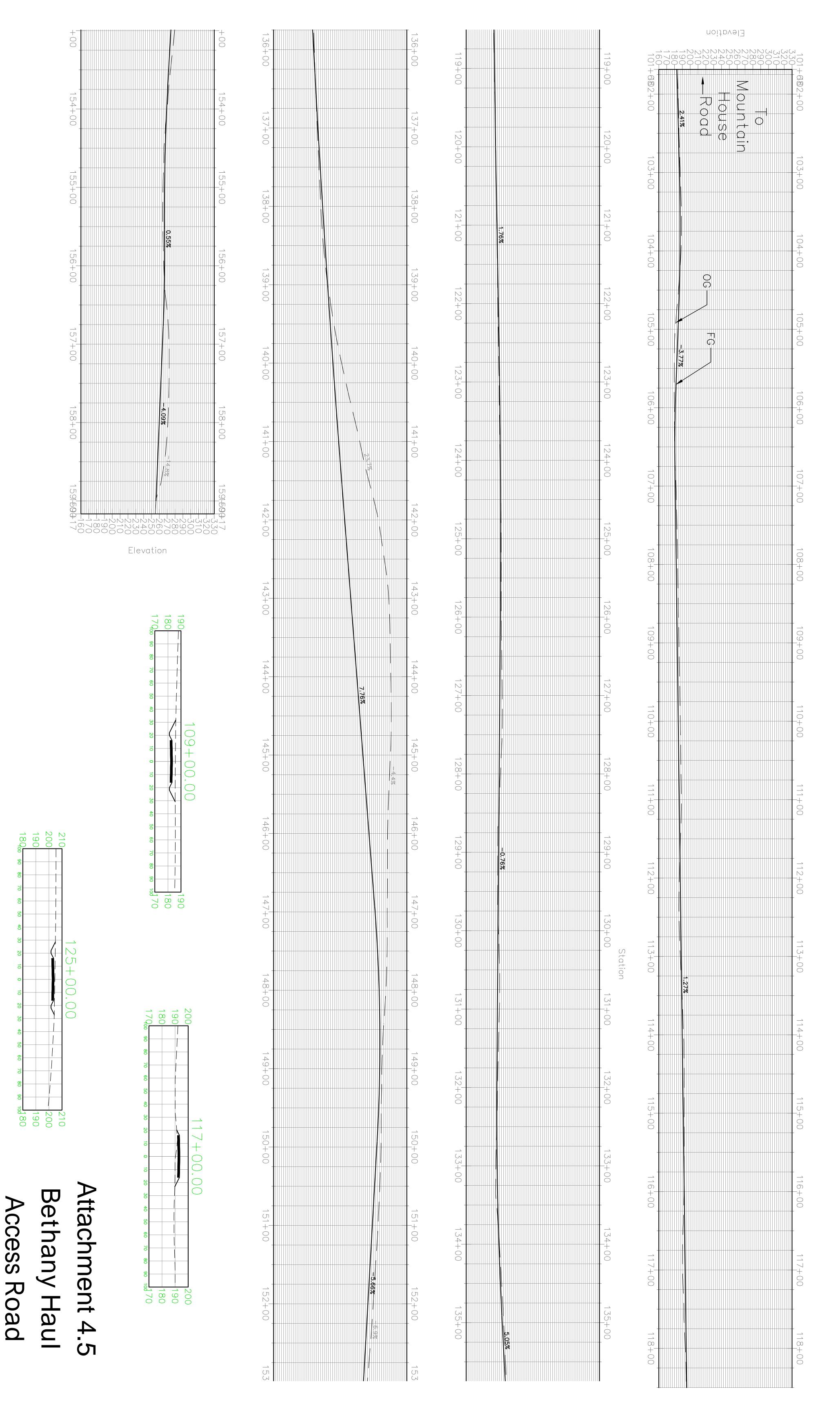
Attachment 4.3
Bethany Haul
Access Road
ALT 2

-220 -210 -200 -190

 \bigcirc

 \bigcup





Current Design